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ANTISUBMARINE ATTACK: COMPUTER
PROGRAM 13-64P

S. A. Denenberg, et al

Center for Naval Analyses
Arlington, Virginia

28 August 1964

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ANTISUBMARINE ATTACK:
COMPUTER PROGRAM 13-64P

By S. A. Dentenberg and
A. Hershaft

Research Contribution No. 60

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Research Contribution
OPERATIONS EVALUATION GROUP
Center for Naval Analyses

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RESEARCH CONTRIBUTION
Operations Evaluation Group

CENTER FOR NAVAL ANALYSES

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ABSTRACT

An IBM 7090 computer program is described which calculates the distribution of distances between the point of activation of a weapon and a moving target submarine taking into account the estimated component attack errors. The model used is more flexible and realistic than similar past efforts and is expected to produce more reliable submarine kill probabilities. The miss distances are computed by Monte Carlo simulation of the actual tracking and firing tactics. They are plotted by an SC 4020 plotter, first in ascending order, then as a cumulative frequency distribution. Flow charts, a listing of the FORTRAN program, and a sample calculation are included.

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I. INTRODUCTION

The determination of the probability of killing an evading submarine has long been a major problem of antisubmarine warfare. Past attack models have been usually restricted to specific tactical situations or sensor/weapon systems and required rather awkward assumptions about the nature of distribution of the various attack component errors.

The effects of antisubmarine weapons as a function of distance are comparatively well known. Therefore, the major difficulty in the determination of kill probabilities lies in the calculation of the probability of placing a weapon within a given distance from the target, in terms of the expected errors in the various stages of attack.

This program provides a distribution of these distances by Monte Carlo simulation of the actual antisubmarine tracking and firing tactics. It is based on a model (reference (a)) which is both flexible enough to cover most tactical situations and sensor/weapon systems and realistic enough to yield reliable kill probability values. The use of the Monte Carlo technique voids the need for unreasonable distortion of component error distributions.

II. GENERAL DESCRIPTION

Model

The tactical situation is shown in figure 1. The attack unit is at the origin of the coordinate system. The true course of the submarine is parallel to the x-axis. At the time $t_1 = 0$, the submarine is at the true point P_1 with polar coordinates $(r_1, \alpha)^*$. The submarine proceeds from P_1 at a speed U_1 and arrives at the point P_2 at time t_2 . It then executes a turn of radius R_t thru γ degrees of arc at a velocity U_2 . When the turn thru γ is completed at time t_3 at point P_3 , the submarine continues on a tangential course at speed U_3 , reaching point P_4 at a depth Z at time t_4 .

The time t_4 is set equal to the actual activation** time of the attack weapon, thus making P_4 a variable position dependent on t_4 . If t_4 is less than t_2 ,

- * All angles are measured from the vertical or the range line, positive direction to the right. Deflections are measured from the range line, positive to the right.
- ** Activation here denotes the step in which the weapon begins to exert its effect on the target (e.g., beginning of search for a homing torpedo or detonation for a depth charge).

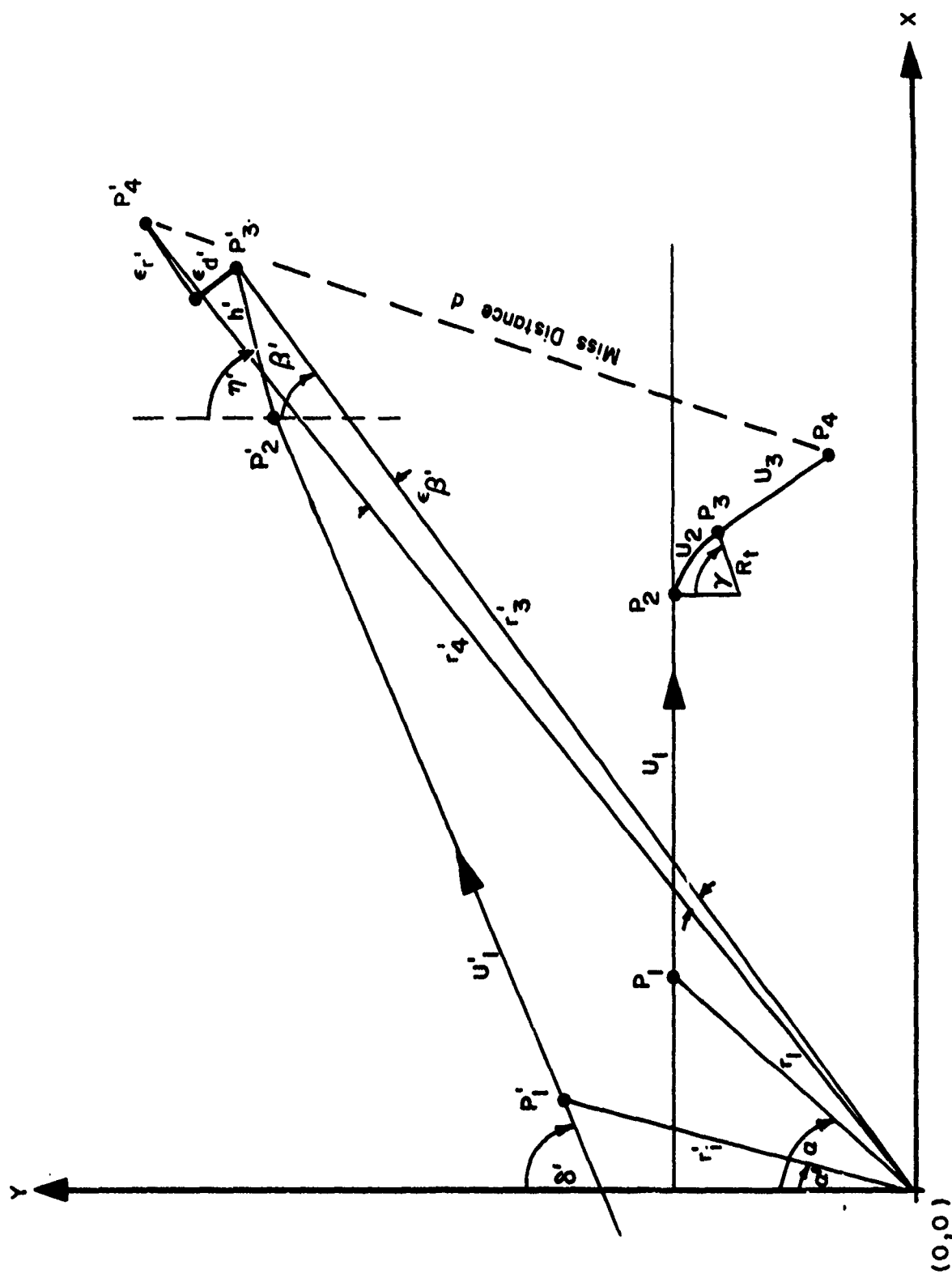


FIGURE 1

P_4 will be somewhere between P_1 and P_2 . If t_4 is greater than t_2 but less than t_3 , P_4 will be somewhere on the circular arc between P_2 and P_3 . Finally, if t_4 is greater than t_3 , P_4 will be located somewhere along the tangent to the circular arc depending on the time elapsed between t_3 and t_4 .

Due to errors in tracking, the attack unit presumes the submarine to be at the point P'_1 with the polar coordinates (r'_1, α') at time $t'_1 = t_1 = 0^*$. The attack unit loses contact with the submarine at P'_1 where it has measured the submarine's speed as U'_1 and its course as δ' . The attacker assumes that the submarine continues from P'_1 at the speed U'_1 on the course δ' and calculates P'_2 , where P'_2 is the assumed location of the submarine at t'_3 , the desired time of activation of the weapon.

The aimpoint of the weapon P'_3 is specified by an offset angle η' and an offset distance h' from the predicted point P'_2 . Due to weapon placement errors, the weapon arrives at the point P'_4 at depth Z' , and activates at time t'_4 . The time t_4 is set equal to t'_4 so that the distance between P_4 and P'_4 becomes the miss distance between the submarine and the weapon.

Program

A miss distance d_i is calculated for each Monte Carlo iteration. At the end of the iteration process, two graphs are plotted:

Graph 1: The miss distances d_i are plotted in sequential ascending order.

Graph 2: The cumulative frequency distribution of the miss distances is plotted as follows: D_M is an input to the program and is used to specify the largest value on the x-axis. If $D_M = 0$ or is not specified, the largest d_i or d_{\max} is found.

D_M is then chosen as the smallest number of the form 1×10^n , 2×10^n , 5×10^n , $-2 \leq n \leq 38$, which is greater than d_{\max} . Once D_M has been chosen, the x-axis of Graph 2 is divided into N_s equal increments, where N_s is also an input to the program.

* Primed variables are used to describe quantities in the observed system. Unprimed variables denote quantities in the true or actual system.

Each increment represents a range of miss distances. The frequency of occurrence for each range of miss distance is calculated and the cumulative frequencies are plotted.

The largest and smallest values of d_i and the number $d_i > D_M$ are printed out. All values of $d_i > D_M$ are ignored; they are not plotted on Graph 1 and they are not used in determining the cumulative frequency distribution of Graph 2.

III. METHOD OF SOLUTION

The inputs for the program consist of the following parameters:

<u>Address</u>	<u>Symbol</u>	<u>Description</u>
1	ID	Identification number which can be assigned to a computer run and which will appear on the graphs and the printed output. ID is an integer such that $0 \leq ID \leq 32,767$
2	N_I	Number of Monte Carlo iterations.
3	D_M	The value of miss distance that will be used as the largest value on the x-axis of Graph 2 (feet)*
4	N_S	Number of equal increments on the x-axis of the cumulative frequency plot (one increment has length = D_M/N_S^{**})
5	N_E	Number of "empty" passes thru random number generators.***
6	r_1	Distance from attack unit to P_1 , the submarine's true position when the last contact is made (feet)
7	Δr_1	Observed position bias error in range (feet)
8	σr_1	One standard deviation of position error in range (feet)

* If not entered, D_M is chosen as the smallest number of the form 1×10^n , 2×10^n , 5×10^n $-2 \leq n \leq 38$ which is greater than the largest calculated miss distance.

** If not entered, N_S will be set equal to 500.

*** N_E passes thru the random number generators are made only for the first data set processed by the program.

<u>Address</u>	<u>Symbol</u>	<u>Description</u>
9	r_t	Radius of turn that submarine executes at P_2 (yards)
10	α	True bearing from attack unit to submarine at point of last contact (degrees)
11	$\Delta\alpha$	Observed position bias error in bearing (degrees)
12	σ_α	One standard deviation of position error in bearing (degrees)
13	γ	Number of degrees of arc in turn of radius r_t .
14	σ_γ	<u>If positive</u> , σ_γ is one standard deviation of error in the turn angle γ (degrees). γ will be replaced by a normal distribution about γ . <u>If negative</u> , γ will be replaced by a uniform distribution from 0 to γ . <u>If zero</u> , γ will not be changed.
15	$\Delta\delta$	Observed course bias error, where true course $\delta = 90$ (degrees)
16	σ_δ	One standard deviation of course error (degrees)
17	u_1	True speed of the submarine from P_1 to P_2 (knots)
18	u_2	True speed of the submarine from P_2 to P_3 (knots)
19	u_3	True speed of the submarine from P_3 to P_4 (knots)
20	Δu_1	Observed bias error of submarine speed u_1 (knots)
21	σ_{u_1}	One standard deviation of error in submarine speed u_1 (knots)
22	t_2	True time at which submarine starts turn (seconds)
23	σ_{t_2}	<u>If positive</u> , σ_{t_2} is one standard deviation of error in the time t_2 (seconds). t_2 will be replaced by a normal distribution about t_2 . <u>If negative</u> , t_2 will be replaced by a uniform distribution from 0 to t_2 . <u>If zero</u> , t_2 will not be changed.
24	t'_3	Desired time of activation of the weapon (seconds)
25	η'	Aimpoint offset angle (degrees)

<u>Address</u>	<u>Symbol</u>	<u>Description</u>
26	h'	Aimpoint offset distance (feet)
27	$\Delta \epsilon_r'$	Weapon placement bias error in range (feet)
28	$\sigma_{\epsilon_r'}$	One standard deviation of weapon placement error in range (feet)
29	$\Delta \epsilon_d'$	Weapon placement bias error in lateral displacement (feet)*
30	$\sigma_{\epsilon_d'}$	One standard deviation of weapon placement error in lateral displacement (feet)*
31	$\Delta \epsilon_\beta'$	Weapon placement bias error in bearing (degrees)*
32	$\sigma_{\epsilon_\beta'}$	One standard deviation of weapon placement error in bearing (degrees)*
33	Z	True depth of submarine when weapon is activated (feet)
34	ΔZ	If σ_Z is positive, ΔZ is considered to be the observed <u>depth bias error</u> (feet). If σ_Z is negative, ΔZ is considered to be the <u>maximum operating depth</u> of the evading submarine (feet).
35	σ_Z	If <u>positive</u> , σ_Z is one standard deviation of error in the depth Z (feet). The observed depth of the submarine, Z' , will be calculated as a normal distribution about $Z + \Delta Z$ (feet). If <u>negative</u> , Z' will be calculated as a uniform distribution from 0 to ΔZ , the maximum operating depth of the submarine (feet). If <u>zero</u> , Z' will be set equal to Z (feet).
36	v'	Velocity of the weapon (feet/seconds).

In the following discussion, R_N is a Gaussian-distributed (mean = 0, standard deviation = 1) random number which is always less than 4 standard deviations. R_U is a uniformly-distributed (mean = 0) random number.

* If $\Delta \epsilon_d' = \sigma_{\epsilon_d'} = 0$, then Option 2 (see page 8) will be used.

If $\Delta \epsilon_\beta' = \sigma_{\epsilon_\beta'} = 0$, then Option 1 (see page 8) will be used.

The miss distance d will be computed once the x-y coordinates of P_4 and P'_4 are determined.

1. It is first necessary to calculate the x and y coordinates of P'_3 . In order to do this, certain variables in the observed system must be computed.

Since r_t , Δu_1 , σ_{u_1} , u_1 , u_2 , and u_3 will be used in subsequent calculations, they must be scaled to be consistent with the units of the rest of the input parameters.

$$U_1 = 1.6878065u_1, \quad i = 1, 2, 3$$

$$\Delta U_1 = 1.6878065\Delta u_1$$

$$\sigma_{U_1} = 1.6878065\sigma_{u_1}$$

$$R_t = 3r_t$$

Then $U'_1 = U_1 + \Delta U_1 + R_{N_1} \sigma_{U_1}$

$$\alpha' = \alpha + \Delta\alpha + R_{N_2} \sigma_{\alpha}$$

$$r'_1 = r_1 + \Delta r_1 + R_{N_3} \sigma_{r_1}$$

$$\delta' = 90 + \Delta\delta + R_{N_4} \sigma_{\delta} \quad (\delta = 90^\circ \text{ in the true system})$$

It is now possible to calculate the x and y coordinates of P'_3 , x'_3 and y'_3 , from the geometry of figure 1.

$$x'_3 = r'_1 \sin\alpha' + U'_1 t'_3 \sin\delta' + h' \sin\eta'$$

$$y'_3 = r'_1 \cos\alpha' + U'_1 t'_3 \cos\delta' + h' \cos\eta'$$

2. The next step is the determination of x'_4 and y'_4 , the x and y coordinates of P'_4 . This calculation depends on how the weapon placement error is described:

Option 1: The weapon placement error is described by range and deflection (ϵ_r , and ϵ_d , respectively)

Option 2: The weapon placement error is described by range and bearing (ϵ_r , and ϵ_β , respectively)

Option 1

$$\epsilon_{r'} = \Delta \epsilon_{r'} + R_{N_5} \sigma_{\epsilon_{r'}}$$

$$\epsilon_{d'} = \Delta \epsilon_{d'} + R_{N_6} \sigma_{\epsilon_{d'}} \quad (\epsilon_{d'} \text{ is measured positive to the right along the range line from the attack unit to the submarine})$$

$$r'_3 = \sqrt{(x'_3)^2 + (y'_3)^2}$$

$$x'_4 = x'_3 + \epsilon_{r'} \frac{x'_3}{r'_3} + \epsilon_{d'} \frac{y'_3}{r'_3} \quad *$$

$$y'_4 = y'_3 + \epsilon_{r'} \frac{y'_3}{r'_3} - \epsilon_{d'} \frac{x'_3}{r'_3} \quad *$$

$$r'_4 = \sqrt{(x'_4)^2 + (y'_4)^2}$$

Option 2

$$\epsilon_{r'} = \Delta \epsilon_{r'} + R_{N_5} \sigma_{\epsilon_{r'}}$$

$$\epsilon_{\beta'} = \Delta \epsilon_{\beta'} + R_{N_6} \sigma_{\epsilon_{\beta'}}$$

$$r'_3 = \sqrt{(x'_3)^2 + (y'_3)^2}$$

$$r'_4 = r'_3 + \epsilon_{r'}$$

$$\beta' = \arctan \frac{x'_3}{y'_3}$$

$$x'_4 = r'_4 \sin (\beta' + \epsilon_{\beta'})$$

$$y'_4 = r'_4 \cos (\beta' + \epsilon_{\beta'})$$

* The derivation of these equations is somewhat lengthy and is therefore not included.

The time of activation of the weapon is calculated taking into account the delay due to weapon placement error.

$$t'_4 = t'_3 + \frac{r'_4 - r'_3}{v}$$

3. The x and y coordinates of P_4 , x_4 and y_4 , must now be determined:

Since t_2 and v will be used in subsequent calculations, they must first be transformed in accordance with the convention defined on page 5.

$$\text{If } \sigma_{t_2} > 0, \text{ then } T_2 = t_2 + R_{N_7} \sigma_{t_2}$$

$$\text{If } \sigma_{t_2} < 0, \text{ then } T_2 = R_{U_1} t_2$$

$$\text{If } \sigma_{t_2} = 0, \text{ then } T_2 = t_2$$

$$\text{If } \sigma_v > 0, \text{ then } \Gamma = v + R_{N_8} \sigma_v$$

$$\text{If } \sigma_v < 0, \text{ then } \Gamma = R_{U_2} v$$

$$\text{If } \sigma_v = 0, \text{ then } \Gamma = v$$

Since T_2 and Γ have now been determined, t_3 is given by:

$$t_3 = T_2 + \frac{\pi}{180} \Gamma \frac{R_t}{U_2}$$

As was noted previously, the location of P_4 is dependent upon t'_4 ; thus, there exist three possibilities:

$$a) t'_4 \leq T_2$$

$$\text{then } x_4 = r_1 \sin \alpha + U_1 t'_4$$

$$y_4 = r_1 \cos \alpha$$

$$b) T_2 < t'_4 \leq t_3$$

$$\text{then let } \theta = \left(\frac{t'_4 - T_2}{t_3 - T_2} \right) \Gamma$$

$$x_4 = r_1 \sin \alpha + U_1 T_2 + R_t \sin \theta$$

$$y_4 = r_1 \cos \alpha - R_t (1 - \cos \theta)$$

$$c) t'_4 > t_3$$

$$\text{then let } S = U_3 (t'_4 - t_3)$$

$$x_4 = r_1 \sin \alpha + U_1 T_2 + R_t \sin \gamma + S \cos \gamma$$

$$y_4 = r_1 \cos \alpha - R_t (1 - \cos \gamma) - S \sin \gamma$$

4. The final step is the calculation of the miss distance:

$$\text{If } \sigma_Z > 0, \text{ then } Z' = Z + \Delta Z + R_{N_9} \sigma_Z^*$$

$$\text{If } \sigma_Z < 0, \text{ then } Z' = R_{U_3} \Delta Z$$

$$\text{If } \sigma_Z = 0, \text{ then } Z' = Z$$

$$\text{Then } d = \sqrt{(x_4 - x'_4)^2 + (y_4 - y'_4)^2 + (Z - Z')^2}$$

* See page 6 to review the definition of σ_Z .

IV. USER'S INSTRUCTIONS

See the list of input parameters on page 4. The user should submit a data submittal form (see appendix C). These forms have space for the submitter's name, the date, the program number (13-64P), the security classification if any, the parameter addresses and values, and an estimate of the computer running time (see section VIII).

Input flexibility has been attained by allowing the user to vary any or all of the parameters in a computer run. In any one set of data the parameters remain fixed, of course, but there is no programmed limit to the number of data sets a user may submit in a run. The only restriction is that each data set must terminate with one blank card, and the last set in the run must terminate with two blank cards.

A further advantage enjoyed by the user is that for each data set after the first, he need submit only those parameter values in a set that are different from those in the previous set.* This is accomplished by identifying each parameter by a unique "address" in the computer memory (see appendix E). Initially every address is cleared to zero so that only non zero input parameters need be entered.

V. SAMPLE PROBLEM

A situation was fabricated for illustrative purposes whereby most of the bias errors were chosen as one percent of the true value and standard deviations were taken as ten percent of the true value. The output is shown in appendix D; and the problem submittal form in appendix C.

VI. KEYPUNCH INSTRUCTIONS

See the list of input parameters on page 4 and the sample problem submittal form in appendix C. Input card formats are described in appendix E.

VII. OPERATOR'S INSTRUCTIONS

Run under control of the Bell System on the IBM 7090 computer. Graphs are made by the Stromberg-Carlson microfilm recorder. A charactron (CRT) tape must be mounted on tape unit A8 in the low-density mode. When the program is run at the David Taylor Model Basin all that is necessary for plotting is a "BCRT" control card (columns 8 thru 12) and the "AMPLOS" subroutine. When the program is run at CEIR, NAVIC or NAVCOSSACT, the "BCRT" control card is not to be used and the "AMPLOS" subroutine is to be replaced by the "CXPLLOT" and "AMPLOF" subroutines; the CRT tape on A8 can then be taken to DTMB or Stromberg-Carlson for processing.

*The exception to this rule is N_E , the number of empty passes through the random number generator (see page 4).

VIII. TIMING

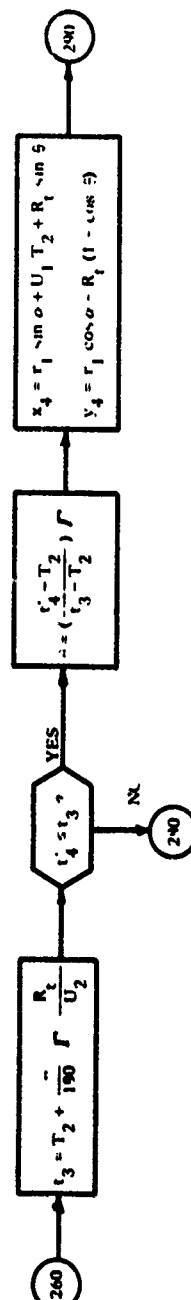
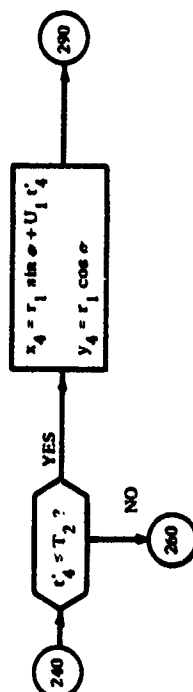
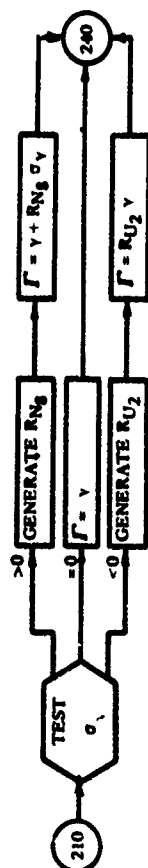
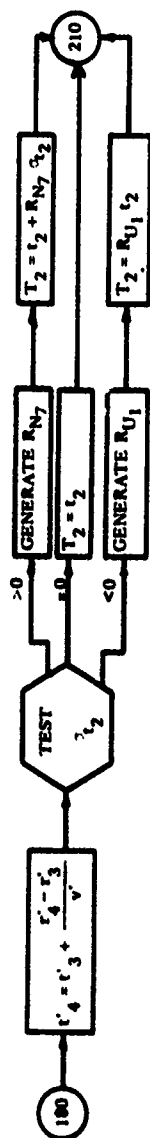
The table presented below gives a conservative estimate of the computer running time for one data set as a function of N_I , the number of Monte Carlo iterations.

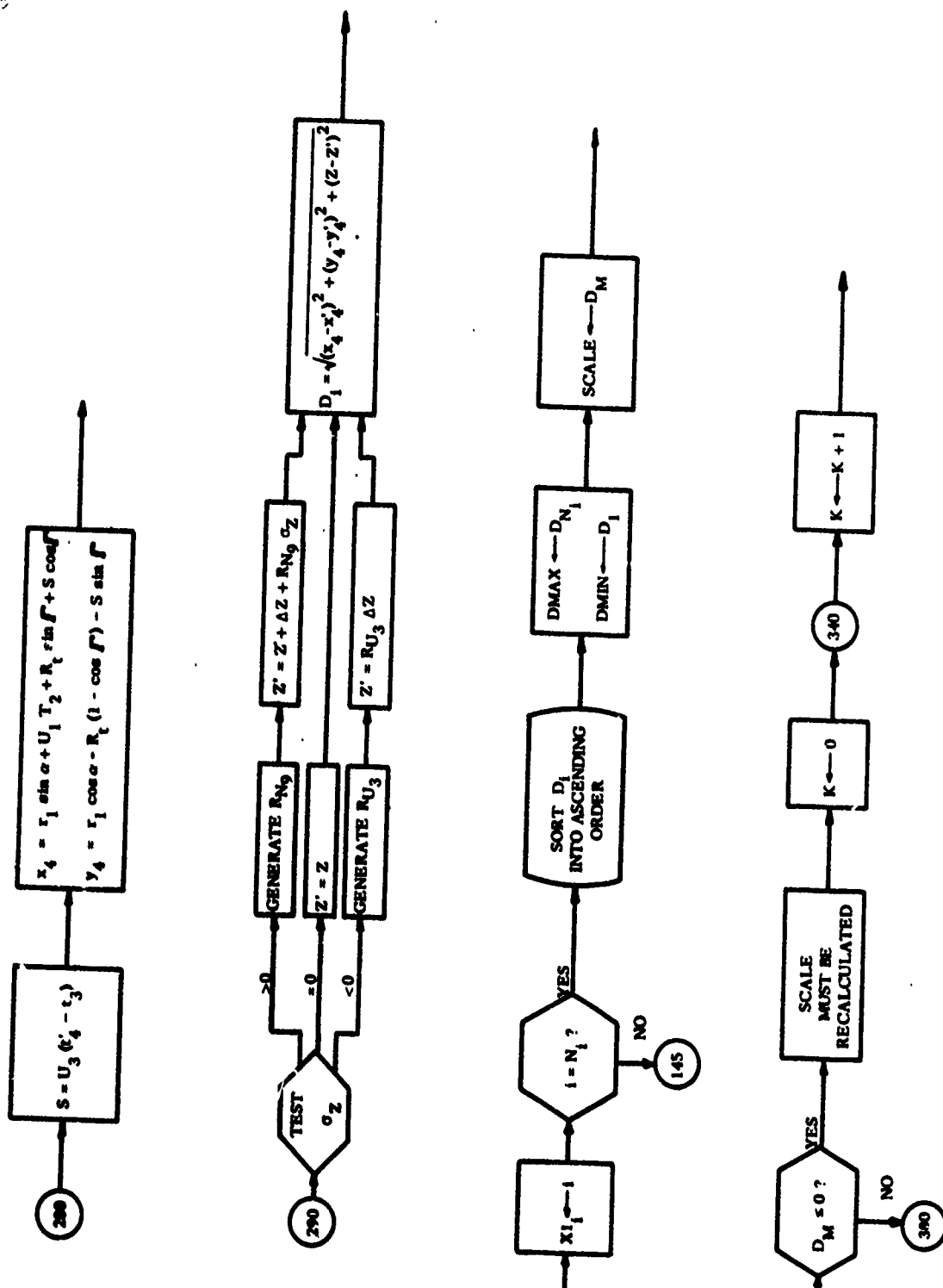
N_I (Number of Monte-Carlo Iterations)	Computer Running Time (in minutes)
100	2
1000	2
2000	3
3000	3
4000	4
5000	5
6000	5
7000	6
8000	6
9000	6

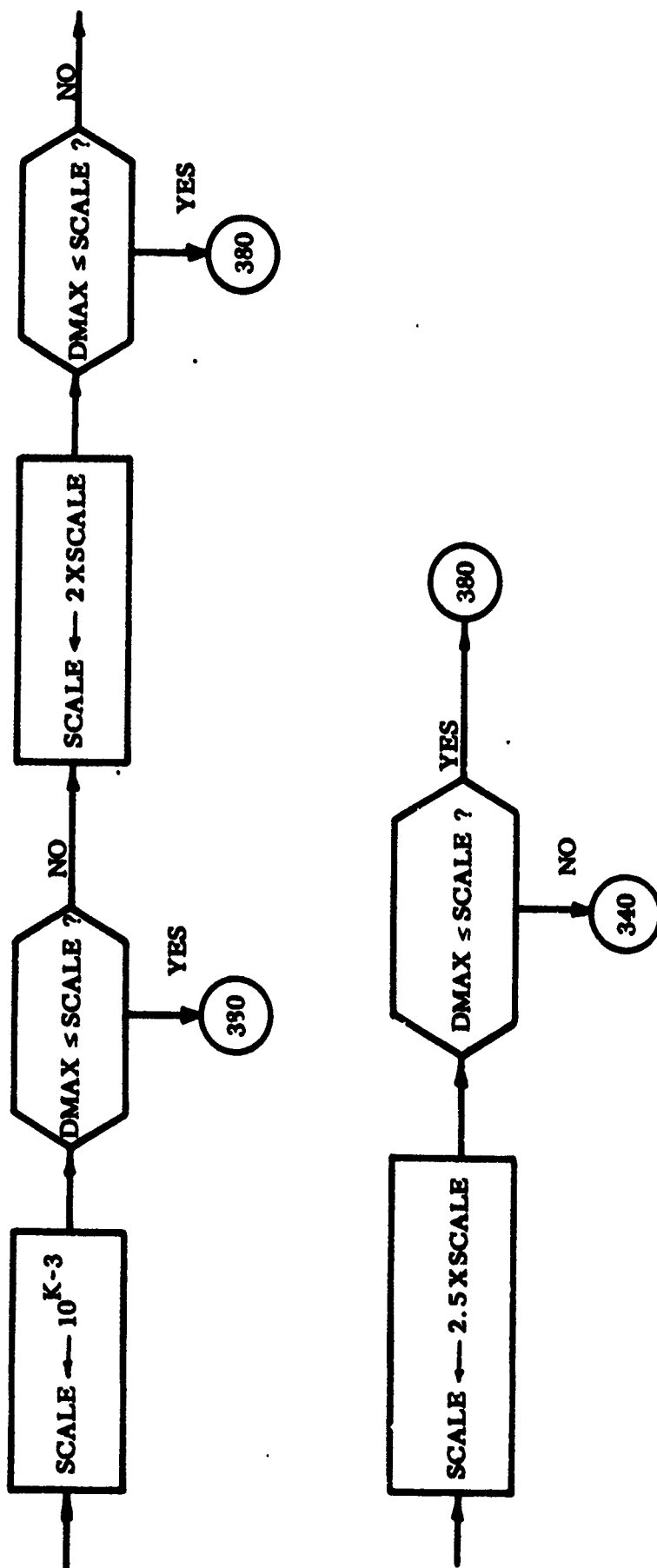
Reference: (a) Operations Evaluation Group, "Design of Antisubmarine Attack Models," in preparation.

[illegible]

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APPENDIX B FORTRAN STATEMENTS

```

COMPUTER PROGRAM 13-64P      ANTI-SUBMARINE ATTACK AH/SAD
      DIMENSION X1(9000),OD(9000),X2(1000),YY(1000),QO(36),G1(12),G2(15)
      EQUIVALENCE (QO(3),DSUBM),(QO(6),R5SUB1),(QO(7),DELR1),(QO(8),SIGRH
X),(QO(9),RTARN),(QO(10),ALPHA),(QO(11),DELALP),(QO(12),SIGALP),
X(QO(13),GAMMA),(QO(14),SIGGAM),(QO(15),DEDEL),(QO(16),SIGDEL),
X(QO(17),U1KNOT),(QO(18),U2KNOT),(QO(19),U3KNOT),(QO(20),DELUA),
X(QO(21),SIGUA),(QO(22),TIME2),(QO(23),SIGT2),(QO(24),T3P),
X(QO(25),ETAP),(QO(26),AITCHP),(QO(27),DELERP),(QO(28),SIGERP),
X(QO(29),DELEDP),(QO(30),SIGEDP),(QO(31),DELEHP),(QO(32),SIGEHP),
X(QO(33),ZEE),(QO(34),DELZ),(QO(35),SIGZ),(QO(36),VPRIME)
      DO 10 I=1,36
10  QO(I)=0.
      KEE=0
      NSUBS=500
      CALL LGCHAR(8.4H SAD)
      PI=3.14159
      G1(12)=740610306060
      G1(11)=275121473060
      G1(10)=016060606060
      G1(9)=603124601360
      G1(7)=606060606060
      G1(6)=443162626024
      G1(5)=316263214523
      G1(4)=256260314560
      G1(3)=216223254524
      G1(2)=314527604651
      G1(1)=242551606060
      G2(15)=741006306060
      G2(14)=G1(11)
      G2(13)=026060606060
      G2(12)=G1(9)
      G2(10)=G1(7)
      G2(9)=236444644321
      G2(8)=633165256026
      G2(7)=512550642545
      G2(6)=237060243162
      G2(5)=635131226463
      G2(4)=314645604626
      G2(3)=604431626260
      G2(2)=243162632145
      G2(1)=232562606060
20  CALL DATA(QO,IND)
      IF(IND)50,50,30
30  PRINT 40
40  FORMAT(1H1)
      CALL LGCHAR(8.4H SAD)
      CALL ENDJOB
50  IDENT=QO(1)
      NSUBI=QO(2)
      NSUBS=QO(4)
      IF(KEE) 52,51,52
51  NEMPTY=QO(5)
52  PRINT 60
60  FORMAT(1H1, 41H CNA PROGRAM 13-64P ANTI-SUBMARINE ATTACK ///
X8H ADDRESS, 5X, 5HVALUE, 11X, 11HDESCRIPTION/)
      GENPTY=NEMPTY
      PRINT 70,(1,QO(I),I=1,4),GENPTY,(1,QO(I),I=6,10)
70  FORMAT(15,F15.4,5X,21HIDENTIFICATION NUMBER/
X15,F15.4,5X,29HNO. OF MONTE-CARLO ITERATIONS/

```

B-1


```

X15.F15.4.5X.35MLARGEST VALUE FOR X-AXIS ON GRAPH 2/
X15.F15.4.5X.37HNUMBER OF EQUAL INCREMENTS ON GRAPH 2/
X5H 5.F15.4.5X.33HNUMBER OF EMPTY RANDOM NO. PASSES/
X15.F15.4.5X.7HR SUB 1/
X15.F15.4.5X.13HDELTA R SUB 1/
X15.F15.4.5X.13HSIGMA R SUB 1/
X15.F15.4.5X.7HR SUB 1/
X15.F15.4.5X.5HALPHA/)
PRINT 80,(1.00(1),I=11,20)
80 FORMAT(15.F15.4.5X.11HDELTA ALPHA/
X15.F15.4.5X.15HSIGMA SUB ALPHA/
X15.F15.4.5X.5HGAMMA/
X15.F15.4.5X.15HSIGMA SUB GAMMA/
X15.F15.4.5X.11HDELTA DELTA/
X15.F15.4.5X.15HSIGMA SUB DELTA/
X15.F15.4.5X.7HU SUB 1/
X15.F15.4.5X.7HU SUB 2/
X15.F15.4.5X.7HU SUB 3/
X15.F15.4.5X.13HDELTA U SUB 1/)
PRINT 90,(1.00(1),I=21,30)
90 FORMAT(15.F15.4.5X.17HSIGMA SUB U SUB 1/
X15.F15.4.5X.7HT SUB 2/
X15.F15.4.5X.17HSIGMA SUB T SUB 2/
X15.F15.4.5X.13HT PRIME SUB 3/
X15.F15.4.5X.9HETA PRIME/
X15.F15.4.5X.7HH PRIME/
X15.F15.4.5X.25HDELTA EPSILON SUB R PRIME/
X15.F15.4.5X.25HSIGMA SUB EPSILON SUB R PRIME/
X15.F15.4.5X.25HDELTA EPSILON SUB U PRIME/
X15.F15.4.5X.25HSIGMA SUB EPSILON SUB D PRIME/)
PRINT 100,(1.00(1),I=31,36)
100 FORMAT(15.F15.4.5X.25HDELTA EPSILON SUB HETA PRIME/
X15.F15.4.5X.32HSIGMA SUB EPSILON SUB BETA PRIME/
X15.F15.4.5X.1HZ/
X15.F15.4.5X.7HDELTA Z/
X15.F15.4.5X.11HSIGMA SUB Z/
X15.F15.4.5X.7HV PRIME////)
IF(NEMPTY) 130,140,110
110 DO 120 I=1,NEMPTY
CALL RANUMH(DUMMY)
120 CALL GRNUM4(DUMMY)
130 NEMPTY=0
140 U1FPS=1.6878065*U1KNOT
U2FPS=1.6878065*U2KNOT
U3FPS=1.6878065*U3KNOT
DELUI=1.6878065*DELUA
SIGUI=1.6878065*SIGUA
RTURN=3.*RTAHN
DO 330 I=1,NSUB1
CALL GRNUM4(RN1)
CALL GRNUM4(RN2)
CALL GRNUM4(RN3)
CALL GRNUM4(RN4)
UIP=U1FPS+DELUI+RN1*SIGUI
ALPHAP=ALPHA+DELALP+RN2*SIGALP
RIP=RSUB1+DELR1+RN3*SIGR1
DELP=90.+DELDEL+RN4*SIGDEL
X3P=RIP*SINDF(ALPHAP)+UIP*T3P*SINDF(DELP)+A1TCHP*SINDF(ETAP)

```

```

Y3P=R1P*COSDF(ALPHAP)+U1P*T3P*COSDF(DELP)+A1TCHP*COSDF(ETAP)
CALL GRNUM4(RN5)
CALL GRNUM4(RN6)
ERP=DELERP+RN5*SIGERP
R3P=SQRTF(X3P**2+Y3P**2)
IF (DELEBP) 170,150,170
150 IF (SIGEBP) 170,160,170
CALCULATIONS FOR OPTION 1
160 EDP=DELEDP+RN6*SIGEDP
X4P=X3P+ERP*X3P/R3P+EDP*Y3P/R3P
Y4P=Y3P+ERP*Y3P/R3P+EDP*X3P/R3P
R4P=SQRTF(X4P**2+Y4P**2)
GO TO 180
CALCULATIONS FOR OPTION 2
170 EBP=DELEBP+RN6*SIGEBP
R4P=R3P+ERP
ANGLE=ATANDF(Y3P/X3P)
IF (X3P) 172,174,174
172 ANGLE=ANGLE+180.
174 BETAP=90.-ANGLE
X4P=R4P*SINDF(BETAP+EBP)
Y4P=R4P*COSDF(BETAP+ERP)
180 T4P=T3P+(R4P-H3P)/VPRIME
TT2=TIME2
IF (SIGT2) 190,210,200
190 CALL RANUM0(RU1)
TT2=RU1*TIME2
GO TO 210
200 CALL GRNUM4(RN7)
TT2=TIME2+RN7*SIGT2
210 GGAMMA=GAMMA
IF (SIGGAM) 220,240,230
220 CALL RANUM0(RU2)
GGAMMA=RU2*GAMMA
GO TO 240
230 CALL GRNUM4(RN8)
GGAMMA=GAMMA+RN8*SIGGAM
240 IF (T4P-TT2) 250,250,260
250 XFOUR=RSUB1*SINDF(ALPHA)+U1FPS*T4P
YFOUR=RSUB1*COSDF(ALPHA)
GO TO 290
260 TIME3=TT2+(PI/180.)*GGAMMA*RTURN/U2FPS
IF (T4P-TIME3) 270,270,280
270 THETA=((T4P-TT2)/(TIME3-TT2))*GGAMMA
XFOUR=RSUB1*SINDF(ALPHA)+U1FPS*TT2+RTURN*SINDF(THETA)
YFOUR=RSUB1*COSDF(ALPHA)-RTURN*(1.-COSDF(THETA))
GO TO 290
280 ESS=U3FPS*(T4P-TIME3)
XFOUR=RSUB1*SINDF(ALPHA)+U1FPS*TT2+RTURN*SINDF(GGAMMA)+ESS*COSDF
X(GGAMMA)
YFOUR=RSUB1*COSDF(ALPHA)-RTURN*(1.-COSDF(GGAMMA))-ESS*SINDF
X(GGAMMA)
290 ZPRIME=ZEE
IF (SIGZ) 300,320,310
300 CALL RANUM0(RU3)
ZPRIME=RU3*DELZ
GO TO 320
310 CALL GRNUM4(RN9)

```

```

ZPRIME=ZEE+DFLZ+RN?SIGZ
320 DD(1)=SQRT((XFOUR-X4P)**2+(YFOUR-Y4P)**2+(ZEE-ZPRIME)**2)
330 X1(1)=1
    CALL FORAST(DD,NSUB1,1)
    DMAX=DD(NSUB1)
    SCALE=DSUBM
    IF (DSUBM) 340,340,380
340 DO 370 K=1,41
    SCALE=.001*10.**K
    IF (DMAX-SCALE) 380,380,350
350 SCALE=2.*SCALE
    IF (DMAX-SCALE) 380,380,360
360 SCALE=2.5*SCALE
    IF (DMAX-SCALE) 380,380,370
370 CONTINUE
380 JJJ=0
    GGG=NSUBS
    DELX=SCALE/GGG
    DO 390 I=1,NSUBS
390 YY(I)=0.
    DO 420 I=1,NSUB1
    INDEX=DD(I)/DELX+0.99999999
    IF (INDEX-NSURS) 410,410,400
400 JJJ=JJJ+1
    GO TO 420
410 YY(INDEX)=YY(INDEX)+1.
420 CONTINUE
    GNORM=NSUB1-JJJ
    X2(1)=DELX/2.
    DO 430 J=2,NSUBS
    X2(J)=X2(J-1)+DELX
    YY(J)=YY(J)+YY(J-1)
430 YY(J-1)=100.*YY(J-1)/GNORM
    YY(NSUBS)=100.*YY(NSUBS)/GNORM
    G1(8)=BINDF(IDENT,6)
    G2(11)=G1(8)
    XUPPER=X1(NSUB1)
    INORM=GNORM
    CALL FNPLT(G1(12),12H(8H NUMBER),29H(23H MISS DISTANCE IN FEET
X),1.,XUPPER,0.,SCALE,20,20,20,1.6H(F5.0),6H(F6.0))
    CALL CURVE(X1(INORM),DD(INORM),INORM,6H
    )
    CALL FNPLT(G2(15),28H(23H MISS DISTANCE IN FEET),13H(9H PERCENT
X),0.,SCALE,0.,100.,20,2,20,1.6H(F6.0),6H(F4.0))
    CALL CURVE(X2(NSUBS),YY(NSUBS),NSUBS,6H
    )
    PRINT 440,DMAX,DD(1),JJJ,SCALE
440 FORMAT(29H THE MAXIMUM MISS DISTANCE = F9.2,5H FEET/29H THE MINIMU
XM MISS DISTANCE = F9.2,5H FEET//12H THERE WERE 14,30H MISS DISTAN
XCES GREATER THAN F9.2,5H FEET)
    KEE=1
    GO TO 20
END

```

APPENDIX C **SAMPLE PROBLEM SUBMITTAL FORM**

OEG COMPUTER DATA SUBMITTAL FORM

Submitted by: J. Doe Date: 1 August 1964
 Program No. 13-64P Est. Time 3 min. Classification Unc1
 Special instructions:

Address	Value	Address	Value	Address	Value	Address	Value
1	1500	21	3				
2	2000	22	100				
3	0	23	10				
4	100	24	500				
5	5	25	45				
6	5000	26	50				
7	50	27	10				
8	500	28	50				
9	100	29	0				
10	20	30	0				
11	.2	31	3				
12	2	32	2				
13	60	33	50				
14	6	34	.5				
15	.9	35	5				
16	9	36	800				
17	30	—	b —				
18	20	—	b —				
19	30						
20	.3						

NOTES:

1. A value of zero must be entered as 0, not left blank.
2. Decimal pts. may be omitted if understood to follow the rightmost digit.
3. The value 3×10^{-5} may be entered as .00003 or 3-5, not as 3×10^{-5} .
4. The factor portion of a value may not contain more than 8 digits.
5. The exponent portion of a value must lie within the range 499.
6. Exponents may be omitted if zero. If not, they must be signed.
7. Blank cards should be indicated by:

C-1
(REVERSE BLANK)

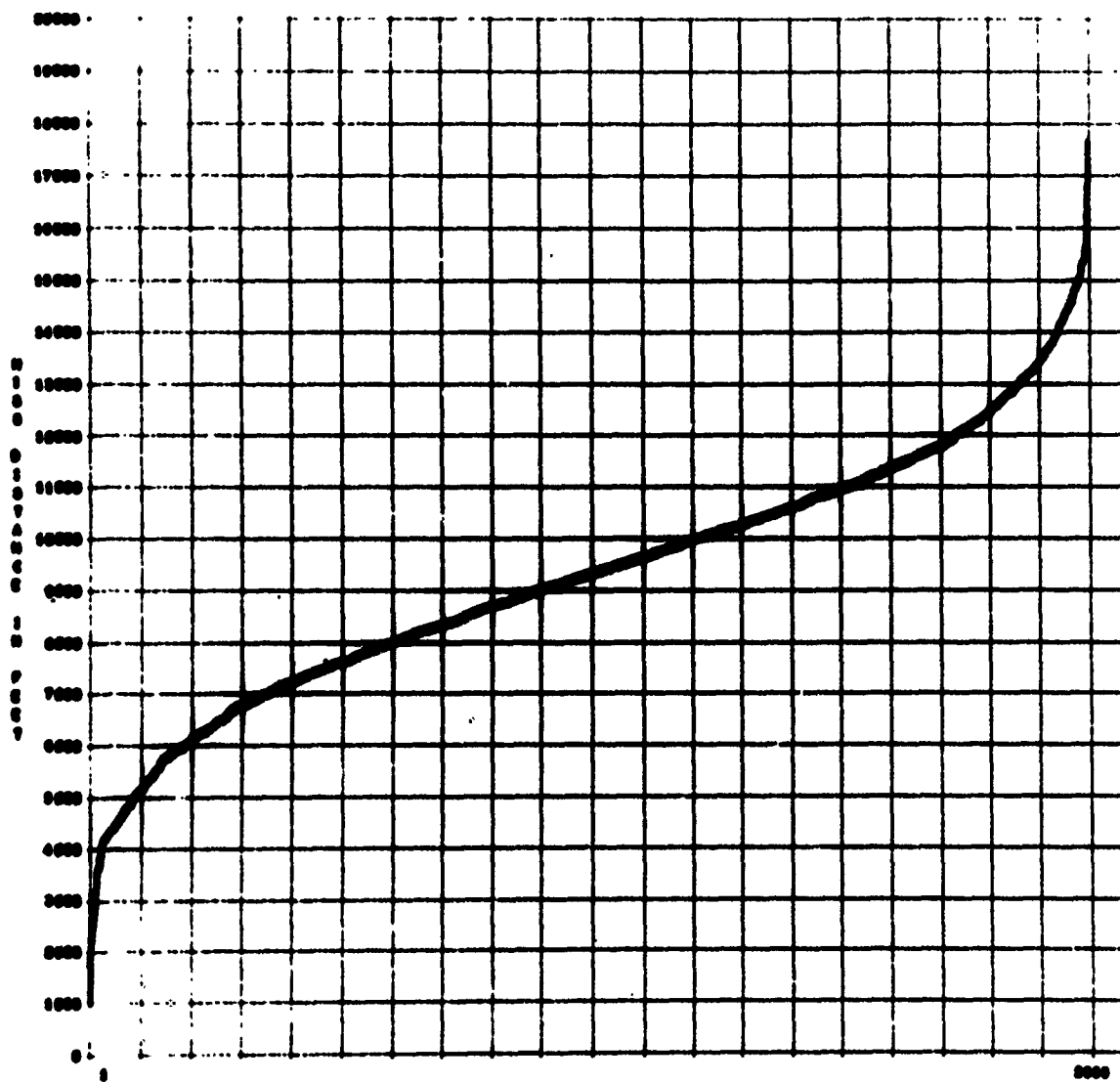
APPENDIX D
SAMPLE PROBLEM OUTPUT
CNA PROGRAM 13-64P ANTI-SUBMARINE ATTACK

ADDRESS	VALUE	DESCRIPTION
1	1500.0000	IDENTIFICATION NUMBER
2	2000.0000	NO. OF MONTE-CARLO ITERATIONS
3	0.	LARGEST VALUE FOR X-AXIS ON GRAPH 2
4	100.0000	NUMBER OF EQUAL INCREMENTS ON GRAPH 2
5	5.0000	NUMBER OF EMPTY RANDOM NO. PASSES
6	5000.0000	R SUB 1
7	50.0000	DELTA R SUB 1
8	500.0000	SIGMA R SUB 1
9	100.0000	R SUB T
10	20.0000	ALPHA
11	0.2000	DELTA ALPHA
12	2.0000	SIGMA SUB ALPHA
13	60.0000	GAMMA
14	6.0000	SIGMA SUB GAMMA
15	0.9000	DELTA DELTA
16	9.0000	SIGMA SUB DELTA
17	30.0000	U SUB 1
18	20.0000	U SUB 2
19	30.0000	U SUB 3
20	0.3000	DELTA U SUB 1
21	3.0000	SIGMA SUB U SUB 1
22	100.0000	T SUB 2
23	10.0000	SIGMA SUB T SUB 2
24	300.0000	T PRIME SUB 3
25	45.0000	ETA PRIME
26	50.0000	H PRIME
27	10.0000	DELTA EPSILON SUB R PRIME
28	50.0000	SIGMA SUB EPSILON SUB R PRIME
29	0.	DELTA EPSILON SUB D PRIME
30	0.	SIGMA SUB EPSILON SUB D PRIME
31	3.0000	DELTA EPSILON SUB BETA PRIME
32	2.0000	SIGMA SUB EPSILON SUB BETA PRIME
33	50.0000	Z
34	0.5000	DELTA Z
35	5.0000	SIGMA SUB Z
36	800.0000	V PRIME

THE MAXIMUM MISS DISTANCE = 17728.80 FEET
 THE MINIMUM MISS DISTANCE = 1012.03 FEET

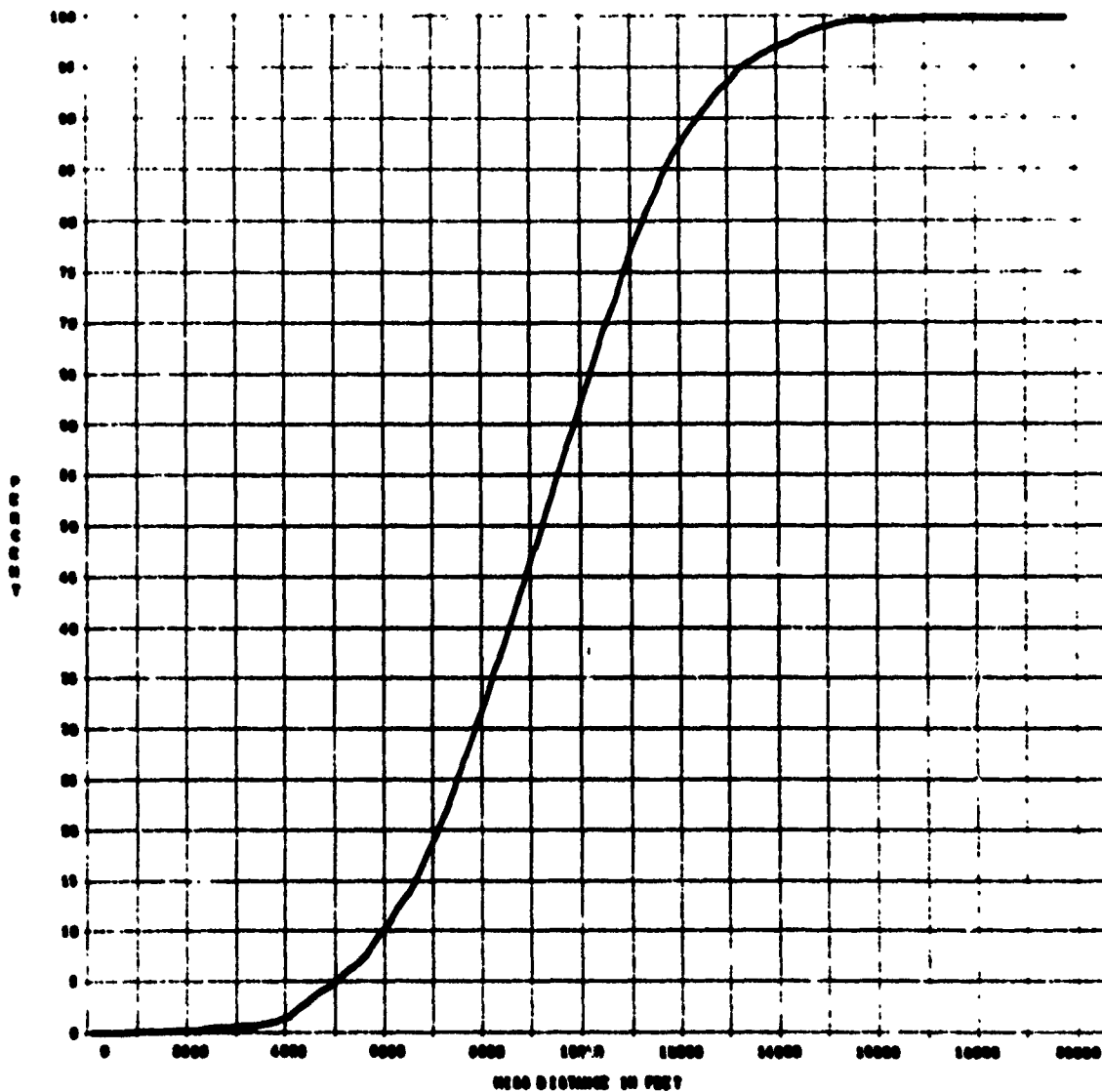
THERE WERE 0 MISS DISTANCES GREATER THAN 20000.00 FEET

D-1



GRAPH 1 D • 1000 AND DISTANCE IN AIRBORNE CRAFT

D-2



GRAPH 2 10 - 100 CUMULATIVE FREQUENCY DISTRIBUTION OF WIND DIRECTION

D-3
(REVERSE BLANK)

APPENDIX E

DATA SUBROUTINE

1. Introduction:

Many computer programs require the flexibility of varying any or all of the parameters in a computer run. Although FORTRAN is fairly flexible in its arithmetic and control statements, its input-output statements are quite rigid. In order to read cards for instance, considerable effort must be expended by the FORTRAN programmer in writing his input statements. This subroutine eliminates some of that tedium. The concept of a "data set" is used. A data set consists of a sequence of punched cards terminated by one blank card. A parameter deck for a computer run may consist of several data sets. Such a parameter deck is terminated by two blank cards.

2. Parameter Addresses:

The primary advantage of this subroutine over FORTRAN input statements results from the use of "parameter addresses." An address is a relative location in the computer memory. It is the subscript of an array or **matrix**. For example, in an array called X, the parameter value X_{53} would be located at address 53. By using the parameter addresses, a user of the program need submit only those parameter values in a data set that are different from those in the previous set.

Three types of addresses are permitted by this subroutine.

- (1) A numeric address consisting of one to five characters, each of which is a digit 0 - 9. Such an address (n) refers to the n^{th} element in a specified array.
- (2) An alpha address consisting of one to six characters, the first of which must be alphabetic (A-Z). The remaining may be alphabetic or numeric (A-Z or 0-9). Such an address refers to the n^{th} element in a specified array ($1 \leq n \leq 26$), where the first character of the address corresponds to n as the 26 letters of the alphabet correspond to the integers 1-26.
- (3) A matrix address consisting of two or more numeric fields separated by commas. For example, the address 53, 47 refers to the element in the 53rd row and the 47th column of a two-dimensional matrix. There is no limit to the number of dimensions in a matrix address.

3. Input Card Format:

A standard submittal form (see attachment) has been designed for the analyst. This form provides for entering parameter values with their associated addresses. The user indicates blank cards to separate data sets. The keypunch operator has the option of punching one address and value per card, or, if the addresses are sequential, of punching one address and several values on a card.

E-1

Only columns 1-72 of a card are used. Each column must contain one of the following: a digit (0-9), a "+" or "-" sign or a dash, a letter (A-Z), a period, a comma, or a blank. Each punched card must contain one parameter address. The address may start in column 1, or, if desired, may start in a later column, provided all columns before it are blank. The address is terminated by at least one blank column. Only one address is permitted on the card. Succeeding columns contain one or more parameter values, each separated by one or more blank columns. A value may be signed or unsigned. The length of the value field is variable. No blanks are permitted within a value field. A value may be punched with or without an exponent. An exponent is recognized by the presence of a plus or minus sign (or dash) between the fractional part and exponent part of the value. Decimal points (periods) may be punched in either the fractional or exponent parts of a value. If more than one value is punched on a card, those after the first will be entered at sequential addresses relative to the address of the first value.

4. Usage:

A data set is read by the use of the statement:

CALL DATA (X, I)

in a FORTRAN program for the IBM 7090. The argument X is the name of an array in the program. The argument I is an indicator set by the subroutine. This indicator may be tested by the main program upon return from the subroutine. It will have a value of 0 or 1 or 2.

- 0: The subroutine has read a data set. The main program will normally proceed to operate on this data.
- 1: The subroutine has read the second blank card which terminates the parameter deck. The main program will normally terminate at this point.
- 2: The subroutine has read a "bad" data card. The main program may terminate the run, or ignore the card and return to the subroutine to read the rest of the data set.

If the cards to be read contain matrix addresses, additional arguments must be included in the FORTRAN calling statement:

CALL DATA (X, D₁, D₂, D₃, ..., D_n, I)

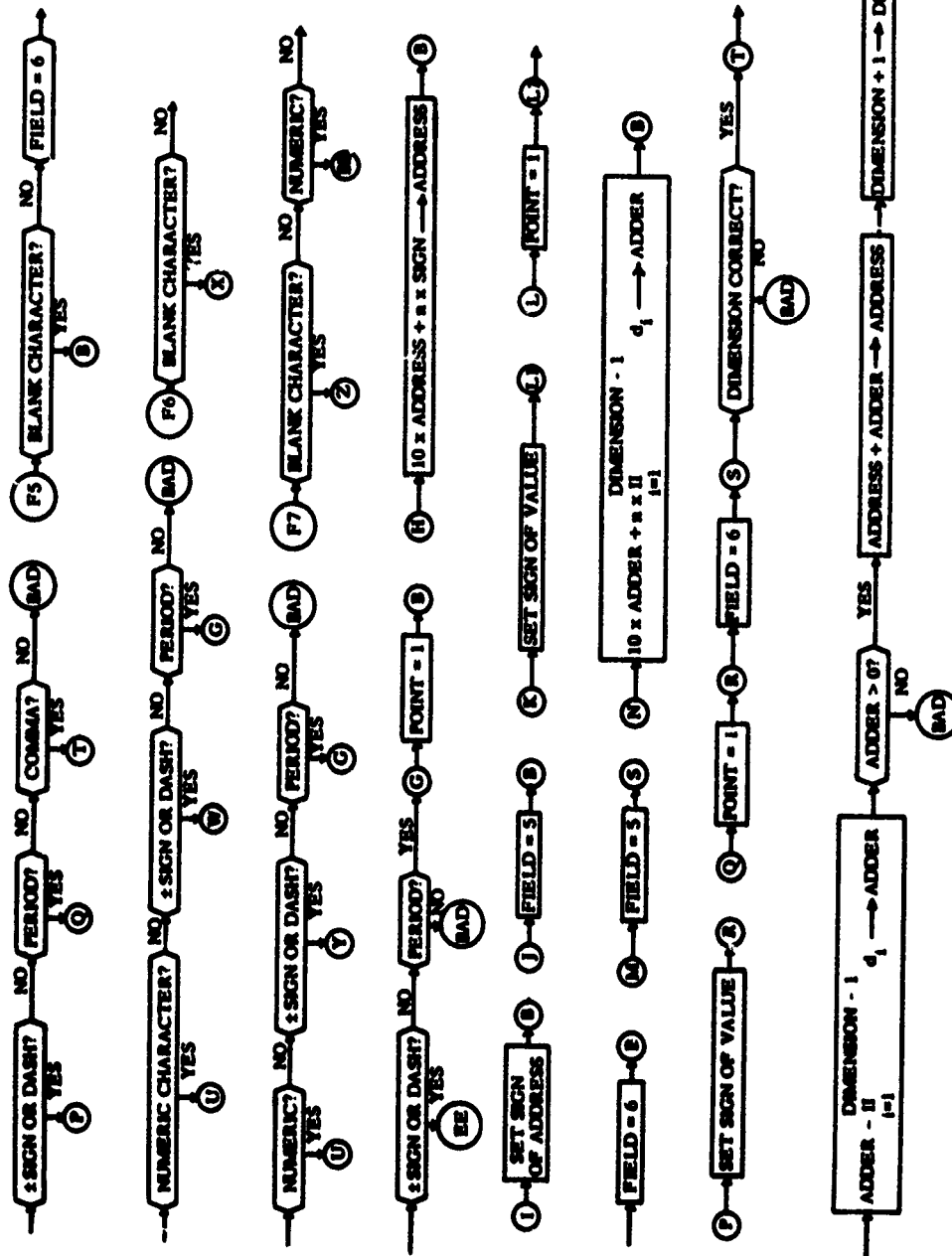
where D_i is the ith dimension of the matrix X.

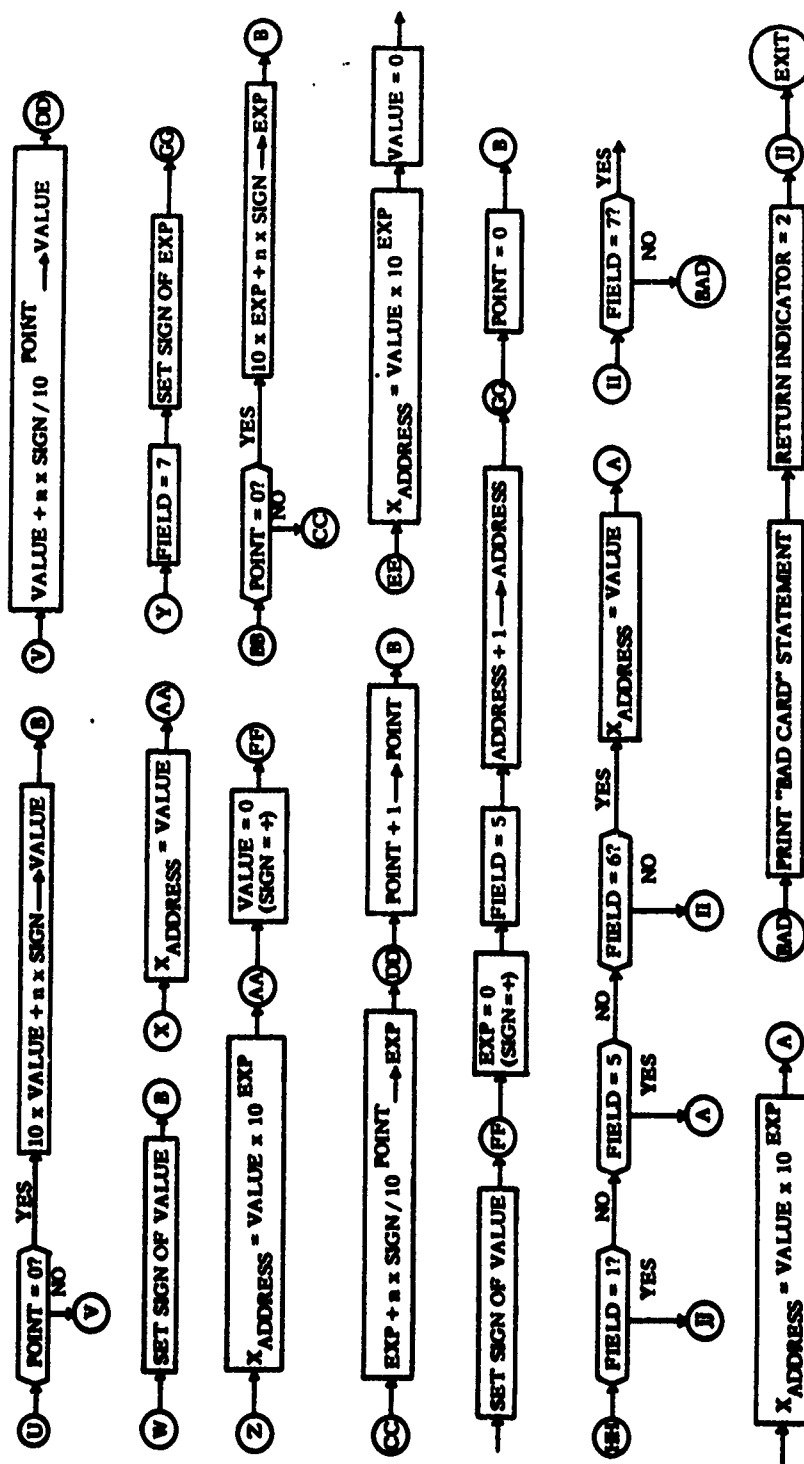
5. Method:

See the attached flow chart. DATA reads parameter values and loading addresses from cards. If sense switch 5 is up, it will read the values and addresses from tape (unit A2). It converts the values to floating point numbers, and stores them as elements of an array specified in the calling statement. The elements are specified by the addresses. If a card (or tape record) is read which contains non-permitted characters (see input card format above), DATA prints the statement "bad data card," followed by an image of the card itself.

6. Coding Information:

See the symbolic listing included in this appendix. DATA is written in the 7090 FAP language. It must be used in conjunction with the BELL system. It requires 401 words storage space.





SYMBOLIC LISTING

	FAP	
	ENTRY DATA	
DATA	SXA X1,1	
	SXA X2,2	
	SXA X4,4	
	CAL 1,4	
	ADD CORE	
	STO XLOC	
	AXT 1,1	
	SXA *+1,1	
	CAL **4	
	ANA MASK	
	TNZ *+2	
	TXI *-4,1,1	
	SXA EXIT,1	
	TXI *+1,1,-1	
	SXA *+1,1	
	CLA **4	
	STA A1	
	STA F1A	
	STA I12	
	AXT 1,1	RETURN INDICATOR = 1
A1	SXD **1	
A	TSX MHREAD,4	READ A CARD
	PZE CARD	
	TRA EXIT	
	TRA BAD	
	STZ ADDRESS	ADDRESS = 0
	STZ VALUE	VALUE = 0
	STZ EXP	EXP = 0
	STZ POINT	POINT = 0
	AXT 1,1	FIELD = 1
	SXA FIELD,1	
	AXT 19,1	
A2	TNX MH,1,1	COLUMN GT 72
	AXT 42,2	
	SXA COLUMN,2	
B	LXA COLUMN,2	COLUMN = COLUMN+1
	TNX A2,2,6	
	SXA COLUMN,2	
	LDO CARD+12,1	
	RQL 36,2	
	PXD 0,0	
	LGL 6	
	STO CHARAC	
	ORA FLOAT	
	FAD FLOAT	
	STO NUMB	
	AXT 42,4	
	CLA CHARAC	
	CAS TABLE+42,4	
	TRA *+2	
	TRA *+3	
	TIX *-3,4,1	

	TRA BAD	
	LXA FIELD,2	
	TRA F1+1,2	
	TRA F7	FIELD=7 (EXPONENT FIELD)
	TRA F6	FIELD=6 (VALUE FIELD)
	TRA F5	FIELD=5 (BLANKS AFTER ADDRESS)
	TRA F4	FIELD=4 (ARRAY ADDRESS)
	TRA F3	FIELD=3 (ALPHA ADDRESS)
	TRA F2	FIELD=2 (NUMERIC ADDRESS)
F1	TXH B,4,41	FIELD=1 (BLANKS BEFORE ADDRESS)
F1A	STZ **	RETURN INDICATOR = 0
	AXT 2,2	FIELD = 2
	SXA FIELD,2	
	TXH H,4,31	NUMERIC CHARACTER
	TXH I,4,28	SIGN OR DASH
	TXL BAD,4,2	
	AXT 3,2	ALPHA CHARACTER, FIELD = 3
	SXA FIELD,2	
	TXI *+1,4,-2	ADDRESS = NTH ALPHA
	SXA ADDRES,4	
	TRA B	
F2	TXH J,4,41	BLANK CHARACTER
	TXH H,4,31	NUMERIC CHARACTER
	TXH K,4,28	SIGN OR DASH
	TXH BAD,4,2	
	TXH L,4,1	PERIOD
	AXT 4,2	COMMA, FIELD = 4
	SXA FIELD,2	
	AXT 2,2	
	SXA DIMENS,2	DIMENSION = 2
	CLA ADDRESS	TEST ADDRESS
	TZE BAD	
	TMI BAD	
F2A	STZ ADDER	ADDER=0
	TRA B	
F3	TXH J,4,41	BLANK CHARACTER
	TXH B,4,31	NUMERIC CHARACTER
	TXH K,4,28	SIGN OR DASH
	TXH B,4,2	ALPHA CHARACTER
	TXH L,4,1	PERIOD
	TRA BAD	
F4	TXH M,4,41	BLANK CHARACTER
	TXH N,4,31	NUMERIC CHARACTER
	TXH P,4,28	SIGN OR DASH
	TXH BAD,4,2	
	TXH Q,4,1	PERIOD
	TRA T	COMMA
F5	TXH B,4,41	BLANK CHARACTER
	AXT 6,2	FIELD = 6
	SXA FIELD,2	
	TXH U,4,31	NUMERIC CHARACTER
	TXH W,4,28	SIGN OR DASH
	TXH BAD,4,2	
	TXH G,4,1	PERIOD

F6	TRA BAD TXH X,4,41 TXH U,4,31 TXH Y,4,28 TXH BAD,4,2 TXH G,4,1 TRA BAD	BLANK CHARACTER NUMERIC CHARACTER SIGN OR DASH PERIOD
F7	TXH Z,4,41 TXH BB,4,31 TXH EE,4,28 TXH BAD,4,2 TXL BAD,4,1	BLANK CHARACTER NUMERIC CHARACTER SIGN OR DASH
G	AXT 1,2 SXA POINT,2 TRA B	PERIOD, POINT = 1
H	LDQ ADDRES MPY H10 XCA ACL CHARAC STO ADDRES TRA B	ADDRESS = 10 X ADDRESS + N
I	TXH B,4,30 CLA ADDRES SSM STO ADDRES TRA B	+ SIGN SET SIGN OF ADDRESS
J	AXT 5,2 SXA FIELD,2 TRA B	FIELD = 5
K	TXH L1,4,30 CLA VALUE SSM STO VALUE TRA L1	+ SIGN SET SIGN OF VALUE
L	AXT 1,2 SXA POINT,2	POINT = 1
L1	AXT 6,2 SXA FIELD,2 TRA B	FIELD = 6
M	AXT 5,2 SXA FIELD,2 TRA S	FIELD = 5
N	LDQ ADDER MPY H10 STQ ADDER TSX T1,4 MPY CHARAC XCA ADD ADDER STO ADDER TRA B	ADDER = 10 X ADDER + N X PROD
P	TXH R,4,30 CLA VALUE SSM	+ SIGN SET SIGN OF VALUE

	STO VALUE	
	TRA R	
Q	AXT 1,2	POINT = 1
	SXA POINT,2	
R	AXT 6,2	FIELD = 6
	SXA FIELD,2	
S	LXA EXIT,2	CHECK DIMENSION
	TXI *+1,2,-3	
	PXA 0,2	
	SUB DIMENS	
	TNZ BAD	
T	TSX T1,4	ADDER=ADDER-PROD
	CLA ADDER	
	SUB PROD	
	STO ADDER	
	TZE BAD	CHECK ADDER
	TMI BAD	
	ADD ADDRES	
	STO ADDRES	
	CLA DIMENS	
	ADD H1	
	STO DIMENS	
	TRA F2A	
T1	SXA T4,4	PROD = PRODUCT OF DIMENSIONS
	CLA H1	
	STO PROD	
	STA T3	
	LXA DIMENS,2	
	TXI *+1,2,-1	
	LXA X4,4	
T2	CAL T3	
	ADD H1	
	STA T3	
T3	CLA **,4	
	STA *+1	
	LDQ **	
	RQL 16	
	MPY PROD	
	STQ PROD	
	TIX T2,2,1	
T4	AXT **,4	
	TRA 1,4	
U	CLA POINT	TEST POINT
	TNZ V	
	LDQ VALUE	VALUE = 10 X VALUE + N
	FMP DEC10	
	SSP	
	FAD NUMB	
	LDQ VALUE	
	LLS 0	
	STO VALUE	
	TRA 8	
V	LXA POINT,4	VALUE = VALUE + N/(10**POINT)
	CLA NUMB	

	FDP DEC10	
	XCA	
	TIX *-2.4.1	
	LDQ VALUE	
	LLS 0	
	FAD VALUE	
	STO VALUE	
	TRA DD	
W	TXH B.4.30	+ SIGN
	CLA VALUE	SET SIGN OF VALUE
	SSM	
	STO VALUE	
	TRA B	
X	CLA XLOC	X(ADDRESS) = VALUE
	SUB ADDRESS	
	STA **2	
	CLA VALUE	
	STO **	
	TRA AA	
Y	AXT 7.2	
	SXA FIELD.2	FIELD = 2
	TXH GG.4.30	+ SIGN
	CLA EXP	SET SIGN OF EXP
	SSM	
	STO EXP	
	TRA GG	
Z	CLA XLOC	X(ADDRESS) = VALUE X 10**EXP
	SUB ADDRESS	
	STA Z1	
	CLA DEC10	
	LDQ EXP	
	CALL EXP(3	
	XCA	
	FMP VALUE	
Z1	STO **	
AA	STZ VALUE	VALUE = 0
	TRA FF	
BB	CLA POINT	TEST POINT
	TNZ CC	
	LDQ EXP	EXP = 10 X EXP + N
	FMP DEC10	
	SSP	
	FAD NUMB	
	LDQ EXP	
	LLS 0	
	STO EXP	
	TRA B	
CC	LXA POINT.4	EXP = EXP + N/(10**POINT)
	CLA NUMB	
	FDP DEC10	
	XCA	
	TIX *-2.4.1	
	LDQ EXP	
	LLS 0	

	FAD EXP	
	STO EXP	
DD	CLA POINT	POINT = POINT + 1
	ADD H1	
	STO POINT	
	TRA B	
EE	CLA XLOC	X(ADDRESS) = VALUE X 10**EXP
	SUB ADDRESS	
	STA EE1	
	CLA DEC10	
	LDQ EXP	
	CALL EXP(3	
	XCA	
	FMP VALUE	
EE1	STO **	
	PXD 0,0	VALUE = 0
	TXH **2,4,30	+ SIGN
	SSM	SET SIGN OF VALUE
	STO VALUE	
FF	STZ EXP	EXP = 0
	AXT 5,2	FIELD = 5
	SXA FIELD,2	
	CAL ADDRESS	ADDRESS = ADDRESS + 1
	ADD H1	
	SLW ADDRESS	
GG	STZ POINT	POINT = 0
	TRA B	
HH	LXA FIELD,1	
	TXL JJ,1,1	FIELD=1, EXIT
	TXL BAD,1,4	
	TXL A,1,5	FIELD=5, READ ANOTHER CARD
	TXH 11,1,6	
	CLA XLOC	FIELD=6, X(ADDRESS) = VALUE
	SUB ADDRESS	
	STA **2	
	CLA VALUE	
	STO **	
	TRA A	
II	TXH BAD,1,7	
	CLA XLOC	FIELD=7,
	SUB ADDRESS	X(ADDRESS) = VALUE X 10**EXP
	STA 111	
	CLA DEC10	
	LDQ EXP	
	CALL EXP(3	
	XCA	
	FMP VALUE	
111	STO **	
	TRA A	
BAD	TSX HPRINT,4	
	PZE PRINT,0,15	
	AXT 2,1	
112	SXD **,1	
X1	AXT **,1	

X2	AXT	**2	
X4	AXT	**4	
EXIT	TRA	**4	
MASK	OCT	777777700000	
PRINT	BCD	3	BAD DATA CARD...
CARD	BSS	12	
ADDRES	HTR	**	
VALUE	HTR	**	
EXP	HTR	**	
POINT	HTR	**	
FIELD	HTR	**	
COLUMN	HTR	**	
TABLE	OCT	60	
	OCT	0	BLANK
	OCT	1	0
	OCT	2	1
	OCT	3	2
	OCT	4	3
	OCT	5	4
	OCT	6	5
	OCT	7	6
	OCT	10	7
	OCT	11	8
	OCT	20	9
	OCT	40	+ SIGN
	OCT	14	- SIGN
	OCT	71	DASH
	OCT	70	Z
	OCT	67	Y
	OCT	66	X
	OCT	65	W
	OCT	64	V
	OCT	63	U
	OCT	62	T
	OCT	51	S
	OCT	50	R
	OCT	47	Q
	OCT	46	P
	OCT	45	O
	OCT	44	N
	OCT	43	M
	OCT	42	L
	OCT	41	K
	OCT	31	J
	OCT	30	I
	OCT	27	H
	OCT	26	G
	OCT	25	F
	OCT	24	E
	OCT	23	D
	OCT	22	C
	OCT	21	B
	OCT	33	A
	OCT	73	PERIOD
			COMMA

CHARAC HTR **
DIMENS HTR **
ADDER HTR **
H10 HTR 10
DEC10 DEC 10.0
H1 HTR 1
PROD HTR **
AMASK OCT 77777
FLOAT OCT 233000000000
NUMB HTR **
XLOC HTR **
CORE OCT 100001
JJ SYN X1
END

OEG COMPUTER DATA SUBMITTAL FORM

Submitted by: _____ Date: _____

Program No. _____ Est. Time _____ Classification _____

Special Instructions:

[illegible]

NOTES:

1. A value of zero must be entered as 0, not left blank.
2. Decimal pts. may be omitted if understood to follow the rightmost digit.
3. The value 3×10^{-5} may be entered as .00003 or 3-5, not as 3×10^{-5} .
4. The factor portion of a value may not contain more than 8 digits.
5. The exponent portion of a value must lie within the range ± 99 .
6. Exponents may be omitted if zero. If not, they must be signed.
7. Blank cards should be indicated by: b .